



MATERIAL BALANCES FOR PROCESSES INVOLVING REACTION

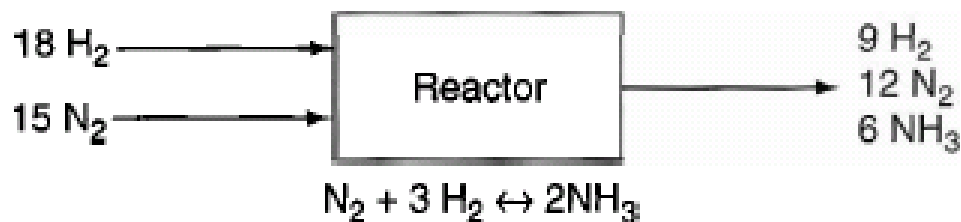


10.1 Species Material Balances

10.1-1 Processes Involving a Single Reaction

$$\left\{ \begin{array}{l} \text{moles of } i \\ \text{at } t_2 \\ \text{in the} \\ \text{system} \end{array} \right\} - \left\{ \begin{array}{l} \text{moles of } i \\ \text{at } t_1 \\ \text{in the} \\ \text{system} \end{array} \right\} = \left\{ \begin{array}{l} \text{moles of } i \\ \text{entering} \\ \text{the system} \\ \text{between } t_2 \text{ and } t_1 \end{array} \right\} - \left\{ \begin{array}{l} \text{moles of } i \\ \text{leaving} \\ \text{the system} \\ \text{between } t_2 \text{ and } t_1 \end{array} \right\} + \left\{ \begin{array}{l} \text{moles of } i \\ \text{generated} \\ \text{by reaction} \\ \text{between } t_2 \text{ and } t_1 \end{array} \right\} - \left\{ \begin{array}{l} \text{moles of } i \\ \text{consumed} \\ \text{by reaction} \\ \text{between } t_2 \text{ and } t_1 \end{array} \right\}$$

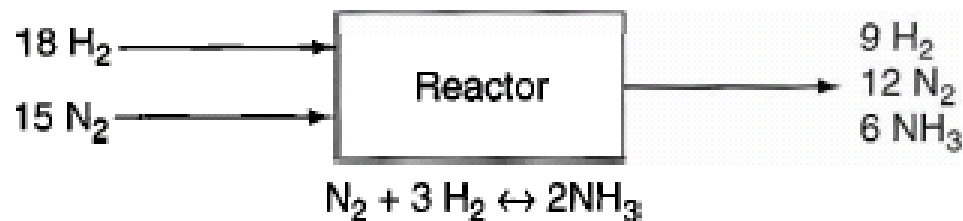
Example:



The process is open, steady-state system operating for 1 min so that the accumulation terms are zero



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NH₃ (generation): $6 - 0 = 6$ g mol

H₂ (consumption): $9 - 18 = -9$ g mol

N₂ (consumption): $12 - 15 = -3$ g mol

$$\xi = \frac{n_i^{out} - n_i^{in}}{\nu_i}$$

and the extent of reaction can be calculated via any species:



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For open system:

$$\xi = \frac{n_i^{\text{out}} - n_i^{\text{in}}}{v_i} \quad i = 1, \dots, N$$

$$\xi = \frac{n_{\text{NH}_3}^{\text{out}} - n_{\text{NH}_3}^{\text{in}}}{v_{\text{NH}_3}} = \frac{6 - 0}{2} = 3$$

$$\xi = \frac{n_{\text{H}_2}^{\text{out}} - n_{\text{H}_2}^{\text{in}}}{v_{\text{H}_2}} = \frac{9 - 18}{-3} = 3$$

$$\xi = \frac{n_{\text{N}_2}^{\text{out}} - n_{\text{N}_2}^{\text{in}}}{v_{\text{N}_2}} = \frac{12 - 15}{-1} = 3$$



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<i>Component</i>	<i>Out</i>	<i>In</i>	=	<i>Generation or Consumption</i>
i	n_i^{out}	$-n_i^{in}$	=	$v_i \xi$
NH ₃ :	6	-0	=	2 (3) = 6
H ₂ :	9	-18	=	-3 (3) = -9
N ₂ :	12	-15	=	-1 (3) = -3

The term $v_i \xi$ corresponds to the moles of i generated or consumed.



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For a closed, unsteady-state system the flows in and out would be zero

$$\xi = \frac{n_i^{final} - n_i^{initial}}{\nu_i}$$

This can be applied to each species that reacts, the resulting set of equations will all contain the extent of reaction . For the species that do not react, $\xi = 0$.



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In terms of the total molar flow in and the total molar flow out:

$$F^{out} = \sum_{i=1}^S n_i^{out}$$

$$F^{in} = \sum_{i=1}^S n_i^{in}$$

where s is the total number of species in the system. The material balance for the total molar flow is:

$$F^{out} = F^{in} + \xi \sum_{i=1}^S \nu_i$$



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If you are given the value of the fraction conversion of the limiting reactant; ξ is related to f by:

$$\xi = \frac{(-f)n_{\text{limiting reactant}}^{\text{in}}}{v_{\text{limiting reactant}}}$$



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Example: The chlorination of methane occurs by the following reaction



You are asked to determine the product composition if the conversion of the limiting reactant is **67%**, and the feed composition in mole % is given as: 40% CH_4 , 50% Cl_2 , and 10% N_2 .



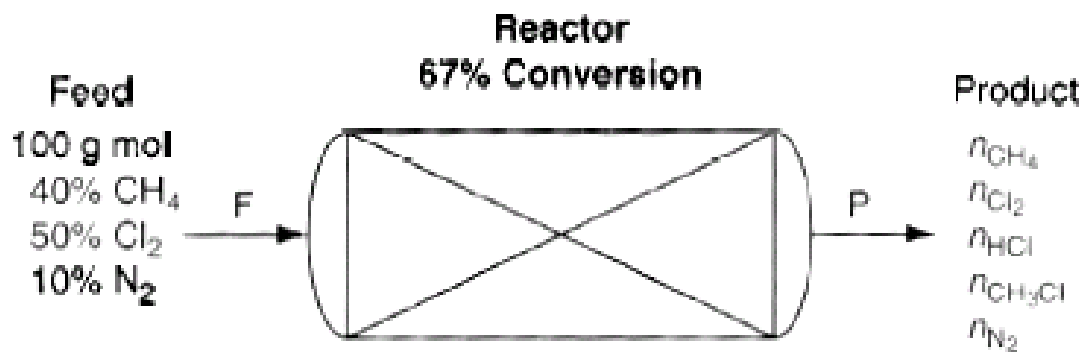
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Solution

Steps 1,2,3, and 4

Assume the reactor is an open, steady-state process. The following figure is a sketch of the process with the known information placed on it.



Step 5

Basis 100 g mol feed



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Step 4

You have to determine the limiting reactant

$$\xi^{\max}(\text{CH}_4) = \frac{-n_{\text{CH}_4}^{\text{in}}}{v_{\text{CH}_4}} = \frac{-40}{(-1)} = 40$$

$$\xi^{\max}(\text{Cl}_2) = \frac{-n_{\text{Cl}_2}^{\text{in}}}{v_{\text{Cl}_2}} = \frac{-50}{(-1)} = 50$$

Therefore, CH_4 is the limiting reactant.

$$\xi = \frac{-f n_{lr}^{\text{in}}}{v_{lr}} = \frac{(-0.67)(40)}{-1} = 26.8 \text{ g moles reacting}$$



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Steps 6 and 7

The next step is to carry out a degree-of-freedom analysis

Number of variables: 11

$$n_{\text{CH}_4}^{\text{in}}, n_{\text{Cl}_2}^{\text{in}}, n_{\text{N}_2}^{\text{in}}, n_{\text{CH}_4}^{\text{out}}, n_{\text{Cl}_2}^{\text{out}}, n_{\text{HCl}}^{\text{out}}, n_{\text{CH}_3\text{Cl}}^{\text{out}}, n_{\text{N}_2}^{\text{out}}, F, P, \xi$$

Number of equations: 1

$$\text{Basis: } F = 100$$

Species material balances: 5





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Specifications: 3

Two of $\{x_{\text{CH}_4}^{\text{in}}, x_{\text{Cl}_2}^{\text{in}}, x_{\text{N}_2}^{\text{in}}\}$ and f (used to calculate ξ)

Implicit equations: 2

$$\sum n_i^{\text{out}} = P \text{ and } \sum n_i^{\text{in}} = F$$

The degrees of freedom are zero.



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Steps 8 and 9

- The species material balances (in moles) give a direct solution for each species in the product:

$$n_i^{out} = n_i^{in} + v_i \xi$$

$$n_{\text{CH}_4}^{out} = 40 - 1(26.8) = 13.2$$

$$n_{\text{Cl}_2}^{out} = 50 - 1(26.8) = 23.2$$

$$n_{\text{CH}_3\text{Cl}}^{out} = 0 + 1(26.8) = 26.8$$

$$n_{\text{HCl}}^{out} = 0 + 1(26.8) = 26.8$$

$$n_{\text{N}_2}^{out} = 10 - 0(26.8) = \underline{10.0}$$

$$100.0 = P$$

- Therefore, the composition of the product stream is: 13.2% CH₄, 23.2% Cl₂, 26.8% CH₃Cl, 26.8% HCl, and 10% N₂



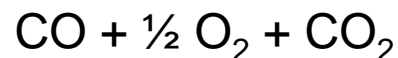
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10.1 -2 Processes Involving Multiple Reactions

- To extend the concept of the extent of reaction to processes involving multiple reactions, you should include in the species material balances only the ξ_i associated with a set of independent chemical reactions called the minimal set of reaction equations.

Example:



Only two of the three equations are independent



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- For open, steady-state processes with multiple reactions, moles for component i :

$$n_i^{\text{out}} = n_i^{\text{in}} + \sum_{j=1}^R v_{ij} \xi_j$$

where

v_{ij} is the stoichiometric coefficient of species i in reaction j in the minimal set.

ξ_j is the extent of reaction for the j th reaction in the minimal set.

R is the number of independent chemical reaction equations (the size of the minimal set).



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- The total moles, N , exiting a reactor are:

$$N = \sum_{i=1}^S n_i^{\text{out}} = \sum_{i=1}^S n_i^{\text{in}} + \sum_{i=1}^S \sum_{j=1}^R v_{ij} \xi_j$$

where S is the number of species in the system.



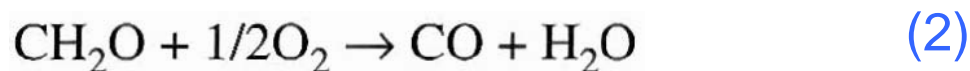
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Example: Formaldehyde (CH_2O) is produced industrially by the catalytic oxidation of methanol (CH_3OH) according to the following reaction:



Unfortunately, under the conditions used to produce formaldehyde at a profitable rate, a significant portion of the formaldehyde reacts with oxygen to produce CO and H_2O , that is,



Assume that methanol and twice the stoichiometric amount of air needed for complete conversion of the CH_3OH to the desired products (CH_2O and H_2O) are fed to the reactor. Also assume that 90% conversion of the methanol results, and that a 75% yield of formaldehyde occurs based on the theoretical production of CH_2O by Reaction 1. Determine the composition of the product gas leaving the reactor.

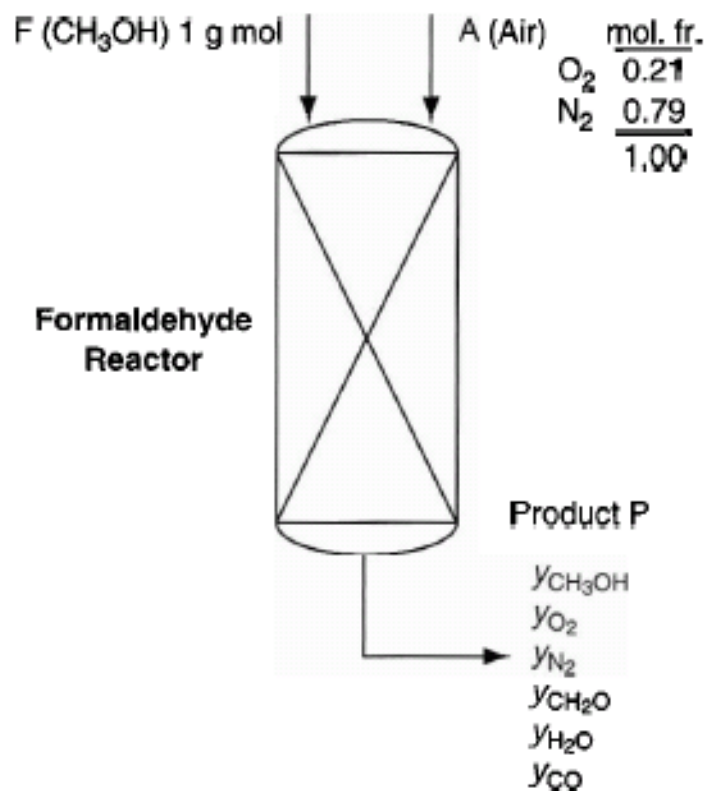


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Solution:

Steps 1,2,3, and 4





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Step 5:

Basis: 1 g mol F

Step 4

You can use the specified conversion of methanol and yield of formaldehyde to determine the extents of reaction for the two reactions. Let ξ_1 represent the extent of reaction 1.

$$\xi = \frac{(-f)n_{\text{limiting reactant}}^{\text{in}}}{\nu_{\text{limiting reactant}}}$$

$$\xi_1 = \frac{-0.90}{-1}(1) = 0.9 \text{ g moles}$$

The yield is related to ξ as follows



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By reaction 1: $n_{\text{CH}_2\text{O}}^{\text{out},1} = n_{\text{CH}_2\text{O}}^{\text{in},1} + 1(\xi_1) = 0 + \xi_1 = \xi_1$

By reaction 2: $n_{\text{CH}_2\text{O}}^{\text{out},2} = n_{\text{CH}_2\text{O}}^{\text{in},2} - 1(\xi_2) = n_{\text{CH}_2\text{O}}^{\text{out},1} - \xi_2 = \xi_1 - \xi_2$

The yield is $\frac{n_{\text{CH}_2\text{O}}^{\text{out},2}}{F} = \frac{\xi_1 - \xi_2}{1} = 0.75$ or $\frac{0.9 - \xi_2}{1} = 0.75$

$\xi_2 = 0.15$ g moles reacting

The amount of air (A) that enters the process. The entering oxygen is twice the required oxygen based on Reaction 1, namely

$$n_{\text{O}_2}^A = 2\left(\frac{1}{2}F\right) = 2\left(\frac{1}{2}\right)(1.00) = 1.00 \text{ g mol}$$



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$$A = \frac{n_{O_2}^A}{0.21} = \frac{1.00}{0.21} = 4.76 \text{ g mol}$$

$$n_{N_2}^A = 4.76 - 1.00 = 3.76 \text{ g mol}$$

Steps 6 and 7

The degree-of-freedom analysis is

Number of variables: 11

$$F, A, P, y_{CH_3OH}^P, y_{O_2}^P, y_{N_2}^P, y_{CH_2O}^P, y_{H_2O}^P, y_{CO}^P, \xi_1, \xi_2$$



MATERIAL BALANCES FOR PROCESSES INVOLVING REACTION



Number of equations: 11

Basis: $F = 1 \text{ g mol}$

Species material balances: 6



Calculated values in Step 4: 3

$$A, \xi_1, \xi_2$$

Implicit equation: 1

$$\sum y_i^P = 1$$



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$$\begin{aligned} P &= \sum_{i=1}^S n_i^{in} + \sum_{i=1}^S \sum_{j=1}^R v_{ij} \xi_j \\ &= 1 + 4.76 + \sum_{i=1}^6 \sum_{j=1}^2 v_{ij} \xi_j \\ &= 5.76 + [(-1) + (-1/2) + (1) + 0 + (1) + 0] 0.9 \\ &\quad + [0 + (1/2) + (-1) + 0 + (1) + (1)] 0.15 = 6.28 \text{ g mol} \end{aligned}$$



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The material balances after entering the values calculated in Step 4 are:

$$n_{\text{CH}_3\text{OH}}^{\text{out}} = y_{\text{CH}_3\text{OH}} (6.28) = 1 - (0.9) + 0 = 0.10$$

$$n_{\text{O}_2}^{\text{out}} = y_{\text{O}_2} (6.28) = 1.0 - (1/2)(0.9) - (1/2)(0.15) = 0.475$$

$$n_{\text{CH}_2\text{O}}^{\text{out}} = y_{\text{CH}_2\text{O}} (6.28) = 0 + 1 (0.9) - 1 (0.15) = 0.75$$

$$n_{\text{H}_2\text{O}}^{\text{out}} = y_{\text{H}_2\text{O}} (6.28) = 0 + 1 (0.9) + 1 (0.15) = 1.05$$

$$n_{\text{CO}}^{\text{out}} = y_{\text{CO}} (6.28) = 0 + 0 + 1 (0.15) = 0.15$$

$$n_{\text{N}_2}^{\text{out}} = y_{\text{N}_2} (6.28) = 3.76 - 0 - 0 = 3.76$$



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10.2 Element Material Balances

- elements in a process are conserved, and consequently you *can not* apply material balance equation (eq.(10.1)) to the elements in a process. Because elements are not generated or consumed, the generation and consumption terms in (eq. (10.1)) can be ignored.



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Example: Hydrocracking is an important refinery process for converting low-valued heavy hydrocarbons into more valuable lower molecular weight hydrocarbons by exposing the feed to a zeolite catalyst at high temperature and pressure in the presence of hydrogen. Researchers in this field study the hydrocracking of pure components, such as octane (C_8H_{18}), to understand the behavior of cracking reactions. In one such experiment for the hydrocracking of octane, the cracked products had the following composition in mole percent: 19.5% C_3H_8 , 59.4% C_4H_{10} , and 21.1% C_5H_{12} . You are asked to determine the molar ratio of hydrogen consumed to octane reacted for this process.

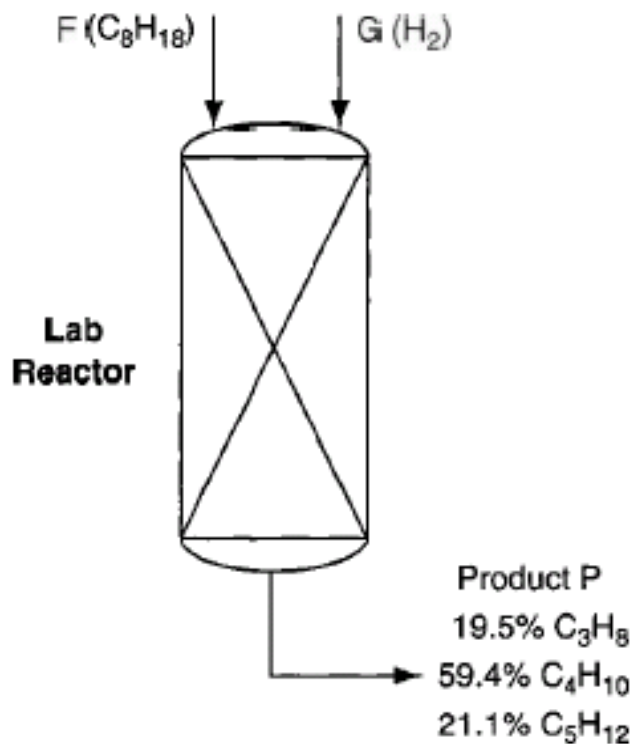


MATERIAL BALANCES FOR PROCESSES INVOLVING REACTION



Solution:

Steps 1,2,3, and 4





MATERIAL BALANCES FOR PROCESSES INVOLVING REACTION



Step 5:

Basis: $P = 100 \text{ g mol}$

Step 6,7:

The degree-of-freedom analysis is

Variables: 3

F, G, P

Equations: 3

Element balances: 2

H, C

Basis: $P = 100$



MATERIAL BALANCES FOR PROCESSES INVOLVING REACTION



Step 8:

The element balances after introducing the specification and basis are:

$$\text{C: } F(8) + G(0) = 100[(0.195)(3) + (0.594)(4) + (0.211)(5)]$$

$$\text{H: } F(18) + G(2) = 100[(0.195)(8) + (0.594)(10) + (0.211)(12)]$$

$$F = 50.2 \text{ g mol}$$

$$G = 49.8 \text{ g mol}$$

$$\frac{\text{H}_2 \text{ consumed}}{\text{C}_8\text{H}_{18} \text{ reacted}} = \frac{49.8 \text{ g mol}}{50.2 \text{ g mol}} = 0.992$$



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10.3 Material Balances involving Combustion

- Combustion is the reaction of a substance with oxygen with the associated release of energy and generation of product gases such as H_2O , CO_2 , CO , and SO_2
- Most combustion processes use air as the source of oxygen, assume that air contains 79% N_2 and 21% O_2 , neglecting the other components and can assume that air has an average molecular weight of 29.



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- In combustion, some terminologies require special attention such as:
- **Flue or stack gas:** all the gases resulting from a combustion process including the water vapor, sometimes known as a wet basis.
 - **Orsat analysis or dry basis:** all the gases resulting from a combustion process not including the water vapor.
 - **Complete combustion:** the complete reaction of the hydrocarbon fuel producing CO_2 , SO_2 , and H_2O .



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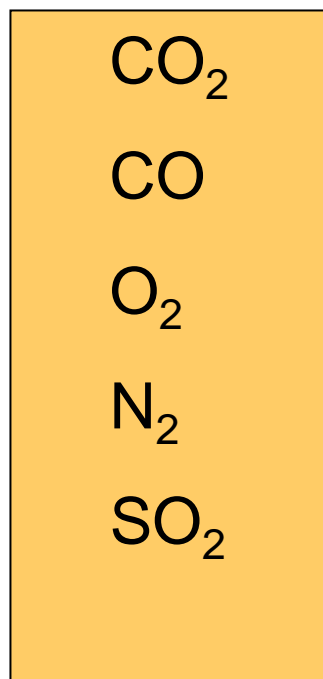
- **Partial combustion:** the combustion of the fuel producing at least some CO.
- **Theoretical air (or theoretical oxygen):** the minimum amount of air (or oxygen) required to be brought into the process for complete combustion. Sometimes this quantity is called the required air (or oxygen).
- **Excess air (or excess oxygen):** in line with the definition of excess reactant given before, excess air (or oxygen) is the amount of air (or oxygen) **in excess of that required for complete combustion.**



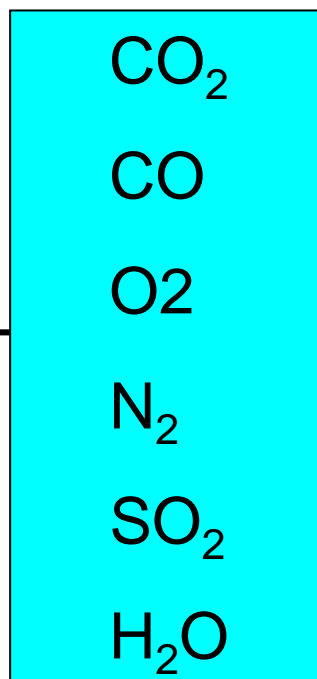
MATERIAL BALANCES FOR PROCESSES INVOLVING REACTION



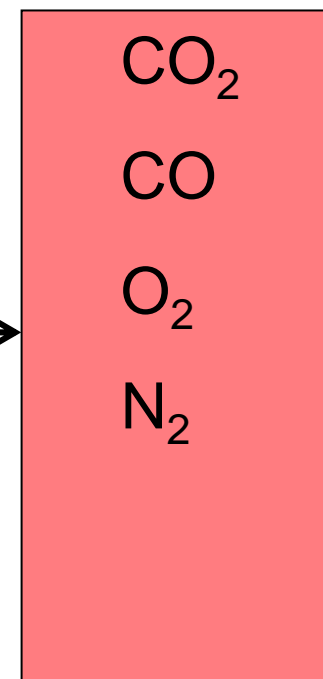
Orsat analysis
dry basis gas



Flue gas
or wet basis



Dry flue gas on
SO₂-free basis





MATERIAL BALANCES FOR PROCESSES INVOLVING REACTION



- **Assumption:** The calculated amount of *excess air* does not depend on how much material is actually burned but what is possible to be burned. Even if only partial combustion takes place, as, for example, C burning to both CO and CO₂, the excess air (or oxygen) is computed as if the process of combustion went to completion and produced only CO₂.
- The percent excess air is identical to the percent excess O₂

$$\% \text{ excess air} = 100 \frac{\text{excess air}}{\text{required air}} = 100 \frac{\text{excess O}_2/0.21}{\text{required O}_2/0.21}$$



MATERIAL BALANCES FOR PROCESSES INVOLVING REACTION



- Percent excess air may also be computed as:

$$\% \text{ excess air} = 100 \frac{\text{O}_2 \text{ entering process} - \text{O}_2 \text{ required}}{\text{O}_2 \text{ required}}$$

Or,

$$\% \text{ excess air} = 100 \frac{\text{excess O}_2}{\text{O}_2 \text{ entering} - \text{excess O}_2}$$



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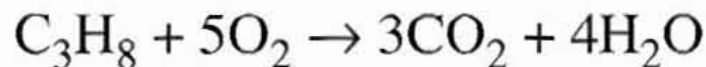
Example: Fuels other than gasoline are being eyed for motor vehicles because they generate lower levels of pollutants than does gasoline. Compressed propane is one such proposed fuel. Suppose that in a test 20 kg of C_3H_8 is burned with 400 kg of air to produce 44 kg of CO_2 and 12 kg of CO. What was the percent excess air?



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Solution:



Basis: 20 kg of C_3H_8

- Since the percentage of excess air is based on the **complete** combustion of C_3H_8 to CO_2 and H_2O , The required O_2 is:

$$\frac{20 \text{ kg } \text{C}_3\text{H}_8}{1 \text{ kg mol } \text{C}_3\text{H}_8} \left| \frac{1 \text{ kg mol } \text{C}_3\text{H}_8}{44.09 \text{ kg } \text{C}_3\text{H}_8} \right| \frac{5 \text{ kg mol } \text{O}_2}{1 \text{ kg mol } \text{C}_3\text{H}_8} = 2.27 \text{ kg mol } \text{O}_2$$

- The entering O_2 is:

$$\frac{400 \text{ kg air}}{29 \text{ kg air}} \left| \frac{1 \text{ kg mol air}}{100 \text{ kg mol air}} \right| \frac{21 \text{ kg mol } \text{O}_2}{100 \text{ kg mol air}} = 2.90 \text{ kg mol } \text{O}_2$$



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- The percentage of excess air is:

$$\% \text{ excess air} = \frac{\text{entering O}_2 - \text{required O}_2}{\text{required O}_2} \times 100$$

$$\% \text{ excess air} = \frac{2.90 \text{ lb mol O}_2 - 2.27 \text{ lb mol O}_2}{2.27 \text{ lb mol O}_2} \left| \frac{100}{1} \right. = 28\%$$



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- In calculating the amount of excess air, remember that the excess is the amount of air that enters the combustion process over and above that required for complete combustion.

Example: A gas containing 80% C_2H_6 and 20% O_2 is burned in an engine with 200% excess air. Eighty percent of the ethane goes to CO_2 , 10% goes to CO . and 10% remained unburned. What is the amount of the excess air per 100 moles of the gas?



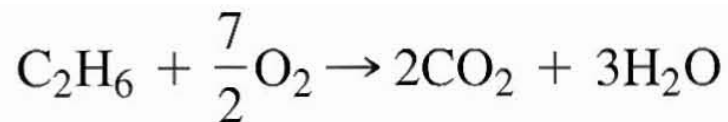
MATERIAL BALANCES FOR PROCESSES INVOLVING REACTION



Solution:

Basis: 100 g mol of gas

- First, you can ignore the information about the CO and the unburned ethane because the basis of the calculation of **excess air is complete combustion**. Specifically C goes to CO₂, S to SO₂, H, to H₂O, CO goes to CO₂, and so on.
- Second, the oxygen in the fuel cannot be ignored. Based on the reaction



- For complete combustion: 80 moles of C₂H₆ require 3.5(80) = 280 moles of O₂



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- The amount of O₂ entering with air = 280 - 20 = 260 moles are needed in the entering air for complete combustion.
- Therefore, 260 moles of O₂ are the required O₂, and the calculation of the 200% excess O₂ (air) is based on 260, not 280, moles of O₂:

<u>Entering with air</u>	<u>Moles O₂</u>
required O ₂ :	260
excess O ₂ (2)(260):	<u>520</u>
total O ₂ (3)(260):	780



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